### Mechatronic

### Motors

### **Mechatronics - energiflow**

#### Structures of the energy conversion system (< 1 h)

- Primary energy to output
- Electrical as intermediate

#### **Power electronic converters as components (**< 3 h)

- AC/DC/AC
- Modulation
- Power Units (50 Hz / SMPS / Integration)
- Passive components / Integration of passives

#### Electromechanical converters as components (< 3 h)

- Conv. machine types
- Elektrostrictive/magnetostrictive converters
- Cooling
- Power and Energy density

#### Energyconvertsre as construction elements (< 1 h)

Laminated steel / powder pressing / injection moulding

#### Powerelectronic measurements (< 2 h)

Current / voltage / flux Torque /speed / position Preassure / flow (in pumps)

### What constitutes a drive?



Schematisk bild av ett positioneringssystem

### Off the shelf, or tailor made?

#### • Off the shelf – complete machine with bearings, housing etc.

- This machine is normally connected to the load via a coupling

#### • Tailor made

- Can be made an integrated part of the driven object.
- Iron core material can be doubly utilized, magnetic conductor and mechanical design element.

### Background

- Most mechanical designs use actuators
- System designs are adapted for "off the shelf"-actuators



## Integrated designs

#### • Integration of actuators requires

- •
  - Actuator design knowledge
  - Production method expertise
- ... and gives
  - Smaller size and lower weight
  - Lower energy consumption
  - Lower EMC-problems
  - Lower cost



# Design task

- 1. Choose geometry
- 2. Estimate response time and dynamics
- 3. Select motor drive
- 4. Calculate electrical power need
- 5. Design power supply
  - 20 V / 200 W trafo available

# System layout



#### There are at least two design flaw's at this stage:

- 1 A standard transformer is used, should be eliminated in the power supply, but is kept for simplification in the power supply design.
- 2 A gear box may not be the best solution, and any alternative drive has not been investigated yet.

## **Power requirements**

- To design the power supply, we need to know the maximum power requirements.
- These come from the drive power and the control electronics power consumption.
- The drive power results from
  - the mechanical work in normal operation
  - the additional work related to speed changes
  - Losses in the gear, motor and power electronics
- To evaluate the drive power, a drive system model in dynamic simulation is convenient to build, for two reasons:
  - It will force us to develop the position and speed controllers
  - It will give us all instantaneous speed and force values to calculate instantaneous mechanical power.

# Details of the power supply

### • Voltage controller

- The current reference is scaled with a full wave rectified sinewave in phase with the line voltage but with unity amplitude.
- Inductor
  - Includes a small resistive voltage drop

#### • Capacitor

– Ideal

#### • Load current

 The load power from the simulation of the mechanical system is use to calculate the load current

# **Power Supply**



# **Mechanical control loop**

• **NB!** We do not model the electrical dynamics at this stage, only the mechanical.



# Details of the mechanical control loop

### • Speed reference generation

- Shift sign of the speed reference every time it hits an end point

#### • Linear to angular speed

- Solve the dynamics in angular speed instead
- Angular speed \* Radius = Linear speed

### • Angular speed control

– PI-controller

#### • Torque source

- Does not respond instantaneously represent as 1'st orde low pass filter
- Has a limited torque capability insert corresponding limitation

### • Pulley and load

– Estimate equivalent intertia

$$\frac{d\omega_{pulley}}{dt} = \frac{T_{pulley} - T_{friction}}{J_{equivalent}}$$
$$T_{friction} = F_{friction} \cdot r_{pulley}$$
$$F_{friction} = -sign(v_{linear}) * 100 [N]$$

### Standard machines

#### • DC machines

- Permanent Magnet
- Series, Shunt and Compound wound

#### • AC servo motors

- Permanent Magnet
- Sinusoidal currents
- Reluctance motors
- Stepper motors

### Electrical Motors properties

### • High torque density

- 1...30 Nm/kg
- Compare combustion motors 1...2 Nm/kg
- Compare Hydraulmotors 600 Nm/kg

### • High efficiency

− ≤ 98%

### Motors Torque and Inertia

<u>One rotor conductor (of all along the airgap surface)</u>:  $F_x = B \cdot i \cdot l$  $T_x = F_x \cdot r = B \cdot i \cdot l \cdot \frac{D}{2}$ 

Total torque along the airgap:  $T = T_x \cdot \pi \cdot D = B \cdot i \cdot l \cdot \frac{D \cdot \pi \cdot D}{2} \propto B \cdot i \cdot rotorvolume$   $P = \omega \cdot T$ 

Inertia

 $J \propto m \cdot r^2$ 

## The $D_{is}^{2}L$ Output Coefficient

• Mechanical power:

$$P_{mech} = \eta_{gap} \cdot P_{gap} = \eta_{gap} \cdot VA_{gap} \cos(\varphi_{gap})$$

$$= \frac{\pi}{2\sqrt{2}} \omega_{mech} k_1 k_{is} (D_{is}^2 l_{is}) B_{g1} K_{s(rms)} \cdot \eta_{gap} \cdot \cos(\varphi_{gap})$$

$$Essen's rule$$

### Servo motor - definition

- Motor for torque, speed or position control
- NB! Line start motors and voltage or frequency controlled motors do not qualify as servo motors.

### DC motors

- Only PM
- Mechanical commutation of rotor currents
- T=k\*ia
- Without current feedback risc for over current at start/reversal and permanent magnet demagnetisation
- Current feedback protects motor AND load



Electro-craft PM-likströmsmotorer



PM-motor i genomskärning

### DC Motor as servo motor

#### • Smaller and smoother rotor

- lower inertia and inductance
- Shorter torque rise time
- Faster acceleration

#### • Skewed rotor

- Smoother torque
- Built in sensors
  - Speed
  - Position







DC-servomotor med takogenerator



### Mathematical model

• Rotor circuit

• Torque 
$$= R_a \cdot i_a + L_a \frac{di_a}{dt} + \omega \cdot \psi_m$$

$$T = \psi_m \cdot i_a$$



### DC motor pros and cons.

- Established
- Soft operation
- High efficiency
- Cheap
- Quiet

- Wear
- Sparking
- EMC

# AC servo motors permanent magnetized

- Winding in th stator
- Electronically commutated
- Position sensor needed
- High torque density







Borstlös synkron servomotor



### Stationary operating point



### AC servo motor pros and cons.

- Soft operation
- High efficiency
- Quiet

- Magnet material expensive
- Small rotor desired magnets difficult (expensive) to mount
- Expensive control electronics
- Position sensor
- Can pick up iron dust, sealed

### Induction motor



Three phase stator

No magnets

Short circuit, "squirrel cage", rotor

Three phase current in the stator

The rotor current must be induced

Three phase power electronics

AM - dynamik

### Utgångsläge

### Flytta statorströmmen snabbt ett steg - vad händer i rotorn?





### Momentegenskaper

$$T = \psi_s \cdot i_r = (\omega - \omega_r) \cdot \frac{\hat{\psi}_s^2}{R_r}$$



### Induction motor pros and cons

- Can start when connected to the public grid
- Robust and reliable
- Cheap
- Simple to maintain
- Standardizsed
- Efficiency
- Power factor

### Stepper Motors

#### • Variable Reluctance

- Rotor is made of only (soft) iron with no magnets but salient teeth

#### • PM stepper motors

- Rotor is made of permanent magnets

#### • Hybrid stepper motors

- Rotor has both teeth and permanent magnets

### Variable reluctance motor

- One winding at a time is energized.
- The rotor takes one "step" at a time



Figure 1. Cross-section of a variablereluctance (VR) motor.

### PM stepper motor

- The electromagnet of the stator and the permanent magnet of the rotor defines specific positions
- By alternating what phase is magnetized, the rotor takes a "step" at a time



Figure 2. Principle of a PM or tin-can stepper motor.

### Stepper motor control

#### • Voltage control mode

- The current is controller by (pre-)selected voltage NO CURRENT FEEDBACK
- Does not work well at higher speeds

#### • Current control mode

- True current feedback is used.

## Stepper motor pros and cons

- Cheap
- No position feedback (that's the idea)
  - Position controlled by counting the number of pulses that is supplied.
- High torque @ low speed

- Noise
- At high acceleration (dynamic) or static load synchronism may be lost. Results in total loss of torque.
- Low torque @ high speed

### Production methods

### • Traditionally:

- Cut, stack and wind
- Many production steps, many parts

#### • Today:

- Press and wind
- Fewer prod steps, fewer parts

#### • Tomorrow

- Mould?
- Single prod step,1 part

# An example of an injection moulded design – in more detail



# TFM: double claw-pole simulated

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| F | VECTOR | FIELDS |
|---|--------|--------|
| • | 120101 |        |

| Quantity            | Value | Unit |
|---------------------|-------|------|
| Inner radius, ri    | 75.0  | mm   |
| Outer radius, ro    | 66.0  | mm   |
| Height of core, hp  | 5.0   | mm   |
| Number of poles, Np | 72    | -    |
| Air-gap, g          | 0.4   | mm   |
| Inner magnet, rpm1  | 66/68 | mm   |
| Outer magnet, rpm2  | 73/75 | mm   |

| Quantity                | Value | Unit              |
|-------------------------|-------|-------------------|
| Pole clearance, Kp      | 0.085 | -                 |
| Tangential tapering, y1 | 2.5   | deg               |
| Axial tapering, y2      | 10    | deg               |
| Progressive radius, cyr | 0.3   | mm                |
| Flank thickness, hf     | 1.4   | mm                |
| Pole thickness, It      | 1.1   | mm                |
| Current density, Jc     | 5     | A/mm <sup>2</sup> |

### Why not before?



#### • In a conventional design the result is poor

- The magnetic flux travels a rather long distance in iron
- Thus, the iron must be a good flux conductor

### Torque

2...3

• Torque = k \* Flux density \* Air gap radius^2 \* Axial length

4...10

• When introducing a low permeability material in a conventional design, the Flux density drops a factor 4...10.

- This leads to low performance
  - That's why no one has considered this before.
- But, if we can increase the air gap radius correspondingly, we can regain the torque